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|--|---|---|---|--|
| $\lambda = \begin{cases} 0,8 & \langle f_{ck} \leq 50 \text{ MPa} \rangle \\ 0,8 - \left(\frac{f_{ck} - 50}{400} \right) & \langle f_{ck} > 50 \text{ MPa} \rangle \end{cases}$ | $\langle f_{ck} \leq 50 \text{ MPa} \rangle$ | $\alpha_c = \begin{cases} 0,85 & \langle f_{ck} \leq 50 \text{ MPa} \rangle \\ 0,85 \left(1 - \frac{f_{ck} - 50}{200} \right) & \langle f_{ck} > 50 \text{ MPa} \rangle \end{cases}$ | $\langle f_{ck} > 50 \text{ MPa} \rangle$ | |
| $F_d = \gamma_f F_k$ | $f_{cd} = \frac{f_{ck}}{\gamma_c}$ | $f_{yd} = \frac{f_{yk}}{\gamma_s}$ | $\beta_s = \frac{\sigma_s}{f_{yd}}$ | $\beta'_s = \frac{\sigma'_s}{f_{yd}}$ |
| $\beta_x = \frac{x}{d} = \frac{\varepsilon_c}{\varepsilon_c + \varepsilon_s}$ | $\beta_y = \frac{y}{d} = \lambda \beta_x$ | $\beta_z = \frac{z}{d} = 1 - 0,5 \lambda \beta_x$ | $\beta_c = \lambda \alpha_c \beta_x \beta_z = \lambda \alpha_c \beta_x (1 - 0,5 \lambda \beta_x)$ | |
| $a_h \geq \max \begin{bmatrix} 2 \text{ cm} \\ \phi_\ell \\ 1,2 d_{\max} \end{bmatrix}$ | $a_v \geq \max \begin{bmatrix} 2 \text{ cm} \\ \phi_\ell \\ 0,5 d_{\max} \end{bmatrix}$ | $a = \begin{cases} 1,00 \ell \\ 0,75 \ell \\ 0,60 \ell \\ 2,00 \ell \end{cases}$ | $b_1 \leq \begin{cases} 0,1a \\ 0,5 b_2 \end{cases}$ | $b_3 \leq \begin{cases} 0,1a \\ b_4 \end{cases}$ |

| vigas de seção retangular <u>com</u> armadura de compressão | | | |
|---|---------------------------|--------------------------------------|--|
| $M_{Rd} = \max \begin{bmatrix} M_{d,min} \\ M_{Sd} \end{bmatrix} = \max \begin{bmatrix} 0,8 W_0 f_{ctk,sup} \\ M_{Sd} \end{bmatrix}$ | $\beta_x = \beta_{x,dtl}$ | $\frac{d'}{d}$ | $\left. \begin{array}{l} \beta_z \\ \beta_c \\ \beta_s \\ \beta'_s \end{array} \right\} \Rightarrow \text{tab}$ |
| $W_0 = \frac{b_w h^2}{6}$ | | | $M_{Rd1} = \beta_c b_w d^2 f_{cd}$ |
| $f_{ctk,sup} = \begin{cases} 0,39 \times \sqrt[3]{f_{ck}^2} & \langle f_{ck} \leq 50 \text{ MPa} \rangle \\ 2,756 \ln(1 + 0,11 f_{ck}) & \langle f_{ck} > 50 \text{ MPa} \rangle \end{cases}$ | | | $M_{Rd2} = M_{Rd} - M_{Rd1}$ |
| $\beta_c = \frac{M_{Rd}}{b_w d^2 f_{cd}} \Rightarrow \text{tab} \begin{cases} \beta_x \\ \beta_z \\ \beta_s \end{cases}$ | | | $A_s = \left[\frac{M_{Rd1}}{\beta_z d} + \frac{M_{Rd2}}{(d - d')} \right] \frac{1}{\beta_s f_{yd}} \geq 0,15\% A_c$ |
| $\beta_x > \beta_{x,dtl} = \begin{cases} 0,450 & \langle f_{ck} \leq 50 \text{ MPa} \rangle \\ 0,350 & \langle f_{ck} > 50 \text{ MPa} \rangle \end{cases}$ | | | $A'_s = \frac{M_{Rd2}}{(d - d') \beta'_s f_{yd}}$ |
| | | | $(A_s + A'_s) \leq 4\% A_c$ |
| | | | $\beta_s = \left(\frac{\lambda \alpha_c b_w d f_{cd}}{A_s f_{yd}} \right) \beta_x + \left(\frac{A'_s}{A_s} \right) \beta'_s$ |
| para vigas de seção retangular <u>sem</u> armadura de compressão, considerar: | | | |
| $\beta_x \leq \beta_{x,dtl}$ | $M_{Rd1} = M_{Rd}$ | $M_{Rd2} = d' = A'_s = \beta'_s = 0$ | |

vigas de seção T sem armadura de compressão - **$y \leq h_f$**

$$M_{Rd} = \max \begin{bmatrix} M_{d,min} \\ M_{Sd} \end{bmatrix} = \max \begin{bmatrix} 0,8 W_0 f_{ctk,sup} \\ M_{Sd} \end{bmatrix}$$

$$M_{Rd,mesa} = \alpha_c (b_f h_f) \left(d - \frac{h_f}{2} \right) f_{cd}$$

$$M_{Rd} \leq M_{Rd,mesa}$$

$$\beta_c = \frac{M_{Rd}}{b_f d^2 f_{cd}} \Rightarrow \text{tab} \begin{cases} \beta_x \\ \beta_y \\ \beta_z \\ \beta_s \end{cases}$$

$$\beta_x \leq \beta_{x,dtl} = \begin{cases} 0,450 & \langle f_{ck} \leq 50 \text{ MPa} \rangle \\ 0,350 & \langle f_{ck} > 50 \text{ MPa} \rangle \end{cases}$$

$$y = \beta_y d \leq h_f$$

$$A_s = \frac{M_{Rd}}{\beta_z d \beta_s f_{yd}} \begin{cases} \geq A_{s,min} = 0,15\% A_c \\ \leq A_{s,max} = 4\% b_w h \end{cases}$$

$$\beta_s = \left(\frac{\lambda \alpha_c b_f d f_{cd}}{A_s f_{yd}} \right) \beta_x$$

vigas de seção T sem armadura de compressão - **$y > h_f$**

$$M_{Rd} = \max \begin{bmatrix} M_{d,min} \\ M_{Sd} \end{bmatrix} = \max \begin{bmatrix} 0,8 W_0 f_{ctk,sup} \\ M_{Sd} \end{bmatrix}$$

$$M_{Rd,mesa} = \alpha_c (b_f h_f) \left(d - \frac{h_f}{2} \right) f_{cd}$$

$$M_{Rd} > M_{Rd,mesa}$$

$$M_{Rd3} = \alpha_c \left[(b_f - b_w) h_f \left(d - \frac{h_f}{2} \right) \right] f_{cd}$$

$$M_{Rd1} = M_{Rd} - M_{Rd3}$$

$$\beta_c = \frac{M_{Rd1}}{b_w d^2 f_{cd}} \Rightarrow \text{tab} \begin{cases} \beta_x \\ \beta_y \\ \beta_z \\ \beta_s \end{cases}$$

$$\beta_x \leq \beta_{x,dtl} = \begin{cases} 0,450 & \langle f_{ck} \leq 50 \text{ MPa} \rangle \\ 0,350 & \langle f_{ck} > 50 \text{ MPa} \rangle \end{cases}$$

$$y = \beta_y d > h_f$$

$$A_s = \left[\frac{M_{Rd1}}{\beta_z d} + \frac{M_{Rd3}}{\left(d - \frac{h_f}{2} \right)} \right] \frac{1}{\beta_s f_{yd}} \begin{cases} \geq A_{s,min} = 0,15\% A_c \\ \leq A_{s,max} = 4\% b_w h \end{cases}$$

$$\beta_s = \left(\frac{\lambda \alpha_c b_w d f_{cd}}{A_s f_{yd}} \right) \beta_x + \left\{ \frac{\alpha_c [(b_f - b_w) h_f] f_{cd}}{A_s f_{yd}} \right\}$$

seção T - W_0

$$A_c = b_w h + (b_f - b_w) h_f$$

$$W_0 = W_{0,w} = \frac{I}{y_w}$$

$$y_w = \frac{(b_f h^2) - [(b_f - b_w)(h - h_f)^2]}{2\{(b_f h) - [(b_f - b_w)(h - h_f)]\}}$$

$$I = \left\{ \frac{b_f h^3 - [(b_f - b_w)(h - h_f)^3]}{3} \right\} - A_c y_w^2$$